

# Fission of U-238 and Pu-239 production in subcritical sets

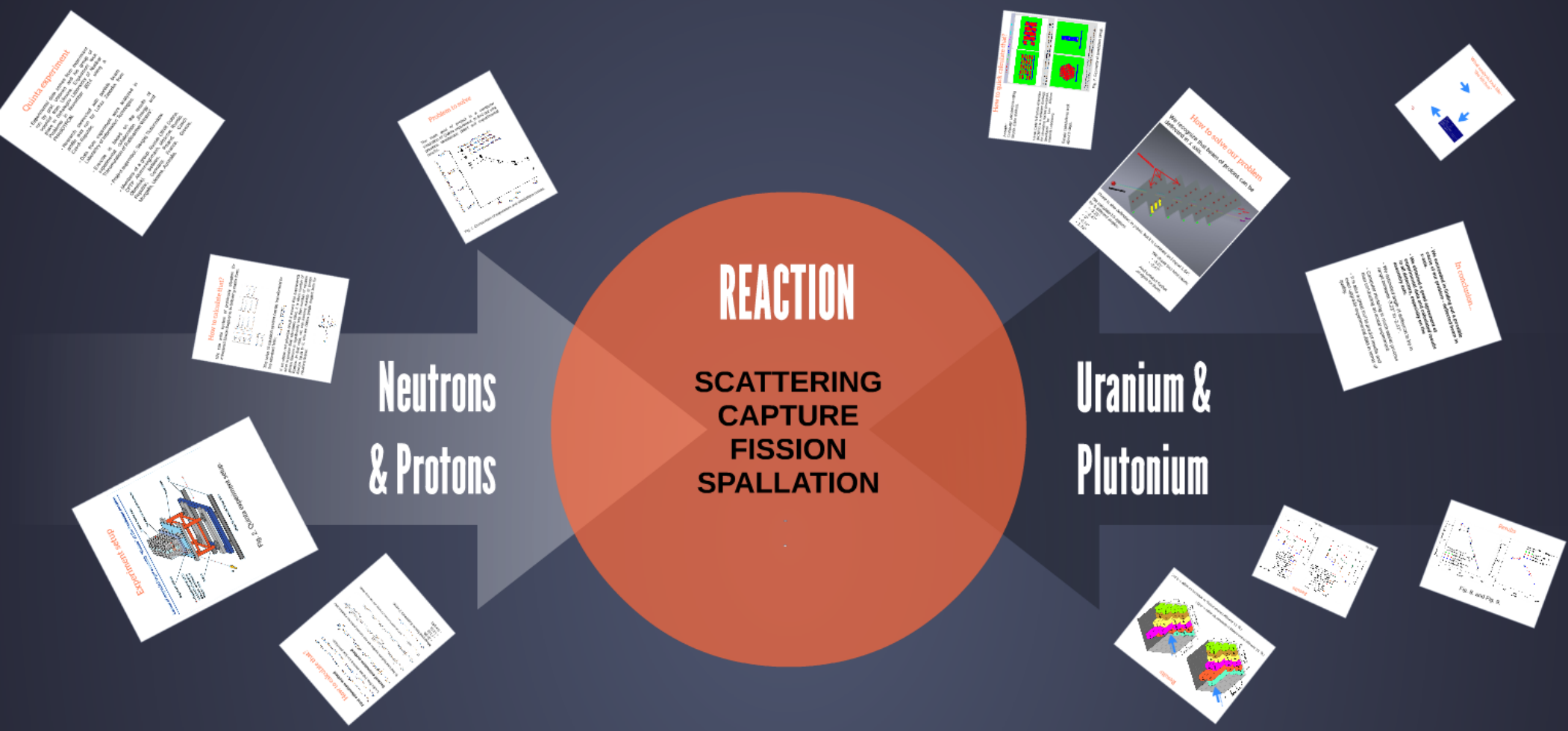
P. Karpowicz, University of Warsaw

M. Konieczny, Warsaw University of Technology

Supervisor:

Andrzej Wojciechowski Ph. D.,

Laboratory of Information Technologies (LIT)



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## Problem to solve

The main goal of project is a computer simulation of Quinta experiment, to find out why previous simulations didn't suit experimental results.

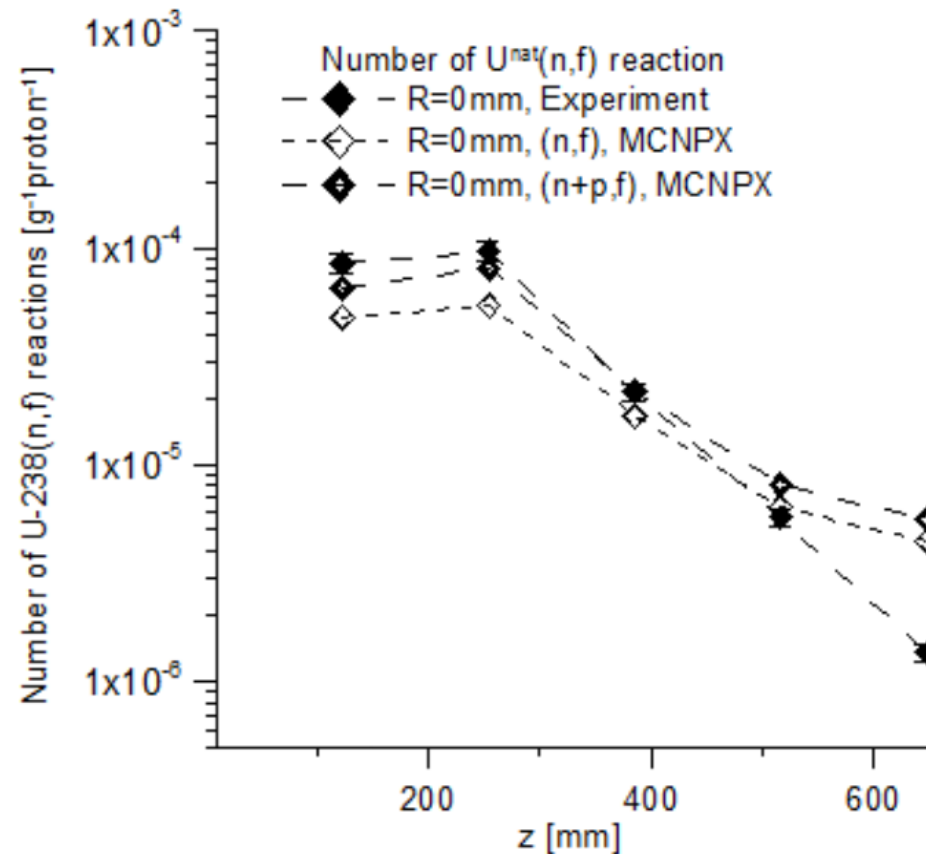


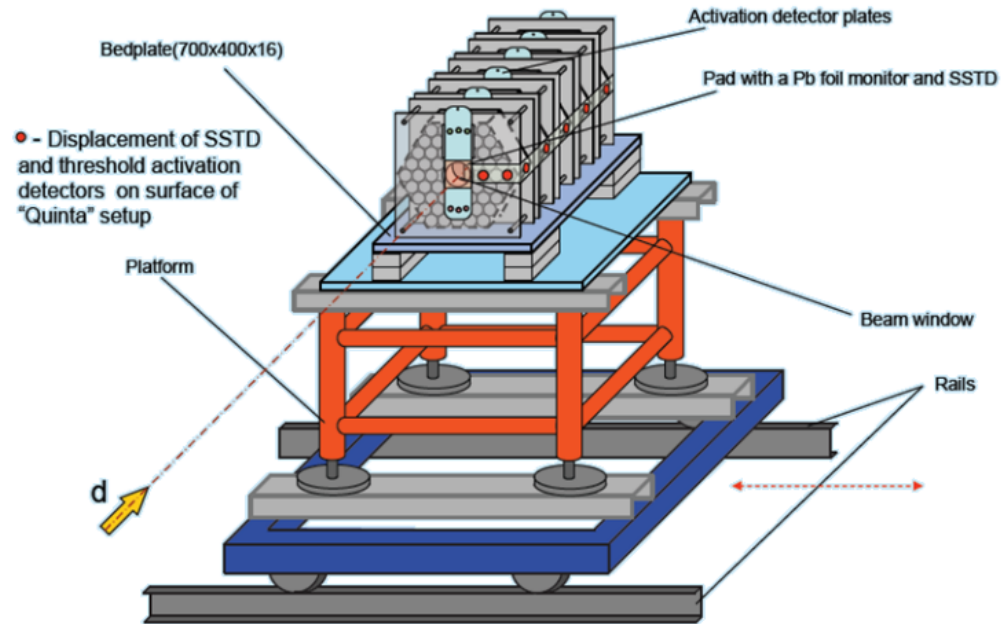
Fig. 1. Comparison of experiment and simulations results.

## Quinta experiment

- Experimental data comes from experiment run by prof. Voronko and his group of scientist from Ukraine. Experiment took place in Dzhelepov Laboratory of Nuclear Problems in November 2014 using a PHASOTRON.
- Research connected with particle beam profile was run by Lukas Zavorka from Czech Republic.
- Data from experiment were analyzed in Laboratory of Information Technologies.
- Exercise is based on the results of experimental collaboration „Energy and Transmutation of Radioactive Wastes”.
- Project supervisor: Siergiej Tiutiunnikov.
- Members of a group: Russia (JINR Dubna, CPTP Atomenergomash, Moscow, Russia, Obmińsk), Belarus, Poland, Czech Republic, Germany, France, Greece, Mongolia, Ukraine, Australia.

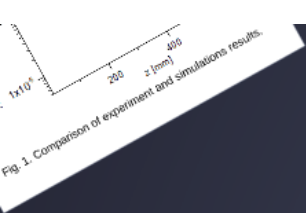
# Experiment setup

## Layout of upgraded target assembly "Quinta" at the irradiation position



ISINN-19, Dubna 25-28 May 2011

Fig. 2. Quinta experiment setup.



There is a  
We calculated  
for 5 different angles  
-3.21°  
-2.47°  
0°  
-0.74°  
-1.74°

ns  
ns

Ura  
Plu

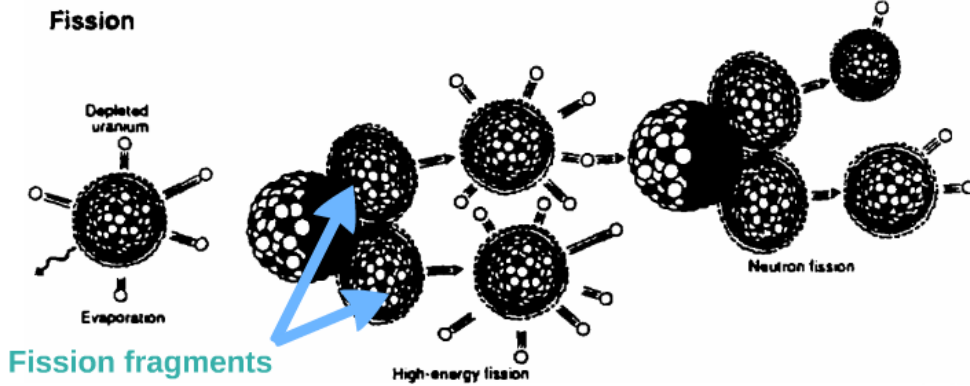
# REACTION

- SCATTERING
- CAPTURE
- FISSION
- SPALLATION



# Fission

Fission is a reaction (decay) of splitting nuclei to lighter parts, with releasing huge amount of energy via neutrons and gamma rays. Reaction can be extorted by neutron flux.



## Fission fragments

High-energy protons bombarding uranium target, high-energy fission competes with evaporation during de-excitation. More neutrons are emitted from high-energy fission than evaporation. Emitted neutrons can go on to induce more fission events.

Fig. 3. Fission scheme.

# Spallation

It's obtained by flux of high energy protons hitting a target (lead, mercury). In effect, nucleus emits several nucleons. Spallation is used to produce high beams of neutrons.

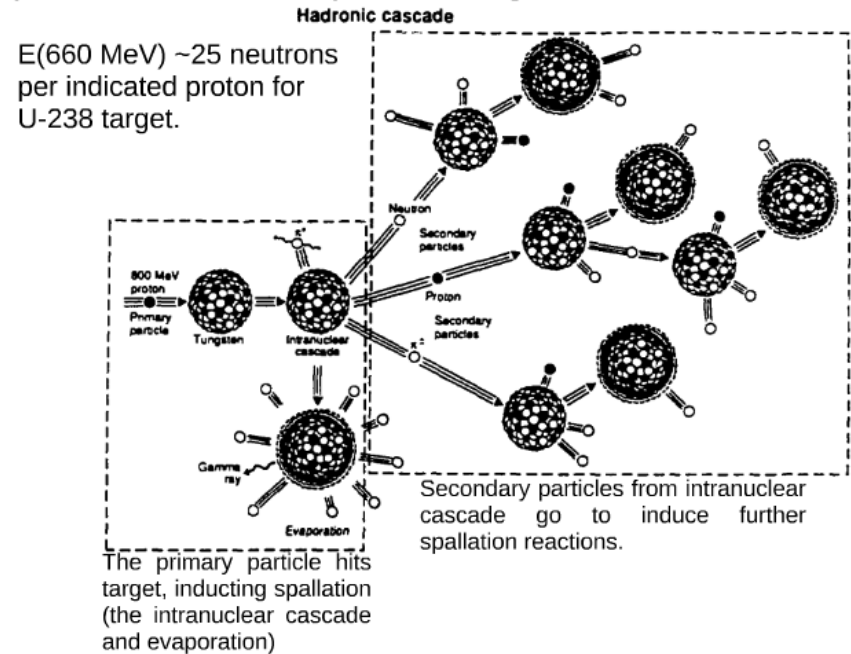


Fig. 4. Spallation scheme.

**Fission and spallation happen in the same nucleus!**

The cross section for U-238(n,f) reaction sharply increase for energies greater than 1 MeV and peaks for energy equal about 50 MeV. It means that to fission U-238 we must produce neutron with energy greater than 10 MeV. (Average energy of fission neutrons is equal to ~2 MeV).

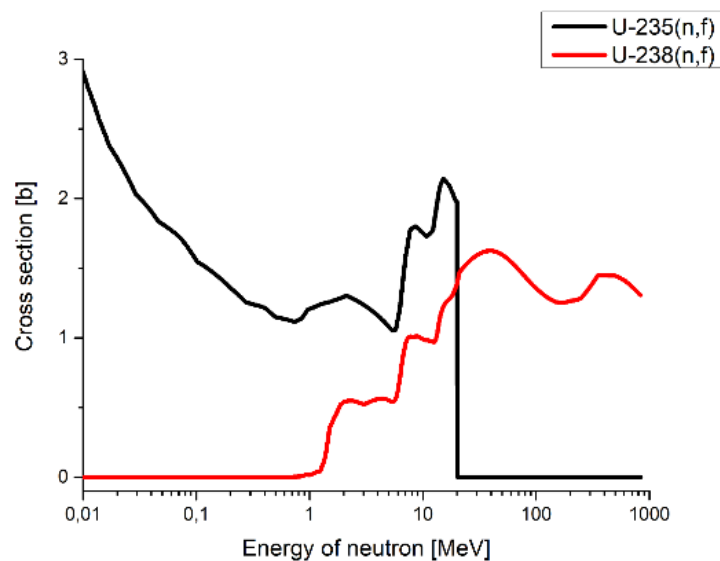


Fig. 5. Cross sections for U-235(n,f) and U-238(n,f).

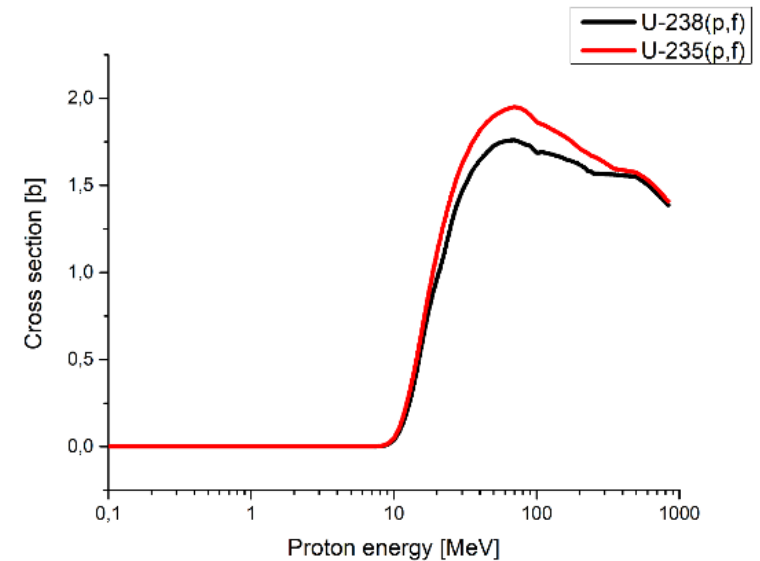


Fig. 6. Cross sections for U-235(p,f) and U-238(p,f).



# How to calculate that?

## First estimation method

$$Y_{U(n,f)Z} = a_{U235} Y_{U235(n,f)Z}(E_n = 25.3\text{MeV}) + a_{U238} Y_{U238(n,f)Z}(E_n = 14\text{MeV})$$

$$Y_{U(n,f)Z} = (Y_{U238(n,f)Z}(E_n = 0.5\text{MeV}) + Y_{U238(n,f)Z}(E_n = 14\text{MeV}))/2$$

Looks fine, but we receive too low precision.

## Second estimation method

$$n_{U(x,f)Z}^{\text{exp}} = \int_0^{\infty} (\phi^n(E) \sigma_{U(n,f)Z}(E) + \phi^p(E) \sigma_{U(p,f)Z}(E)) \rho \frac{A}{m} dE$$

To find total fissions number we can convert previous equation into:

$$n_{U(x,f)Z}^{\text{exp}} = \int_0^{\infty} (\phi^n(E) \sigma_{U(n,f)}(E) \frac{\sigma_{U(n,f)Z}(E)}{\sigma_{U(n,f)}(E)} + \phi^p(E) \sigma_{U(p,f)}(E) \frac{\sigma_{U(p,f)Z}(E)}{\sigma_{U(p,f)}(E)}) \rho \frac{A}{m} dE$$

$$n_{U(x,f)Z}^{\text{exp}} = \int_0^{\infty} (\phi^n(E) \sigma_{U(n,f)}(E) Y_{U(n,f)Z} + \phi^p(E) \sigma_{U(p,f)}(E) Y_{U(p,f)Z}) B dE$$

If  $Y_{U(p,f)Z}$  and  $Y_{U(n,f)Z}$  are constant function of energy one can easy obtain:

$$n_{U(x,f)Z}^{\text{exp}} = Y_{U(n,f)Z} n_{U(n,f)} + Y_{U(p,f)Z} n_{U(p,f)}$$

Measured fission fragments Z were:

- Zr-90
- I-131
- I-133
- Ce-143

## How to calculate that?

We can write system of previously equation for measured fission fragments in following matrix form:

$$\begin{bmatrix} n_{Zr97}^{\text{exp}} \\ n_{I131}^{\text{exp}} \\ n_{I133}^{\text{exp}} \\ n_{Ce143}^{\text{exp}} \end{bmatrix} = \begin{bmatrix} Y_{Zr97,U(n,f)} & Y_{Zr97,U(p,f)} \\ Y_{I131,U(n,f)} & Y_{I131,U(p,f)} \\ Y_{I133,U(n,f)} & Y_{I133,U(p,f)} \\ Y_{Ce143,U(n,f)} & Y_{Ce143,U(p,f)} \end{bmatrix} \begin{bmatrix} n_{U(n,f)} \\ n_{U(p,f)} \end{bmatrix}$$

$$\left. \begin{array}{l} n_{U(n,f)} \geq 0 \\ n_{U(p,f)} \geq 0 \end{array} \right\}$$

The solve of equation system can be transformed to the standard form:

$$\bar{n} = (\bar{Y}^T \bar{Y})^{-1} \bar{Y}^T \bar{n}^{\text{exp}}$$

If we obtain non-physical result it means that experimental error is greater than calculated value. It is when number of proton fissions is significantly less than number of neutron fissions. In that case, we can assume number of proton fissions equal to 0, and we obtain simple explicit form for neutrons fission:

$$n_{U(n,f)} = \frac{\sum_z^4 Y_z n_z^{\text{exp}}}{\sum_z^4 Y_z^2}$$

## How to quick calculate that?

Answer:  
Computer calculations using  
Monte-Carlo method.

Monte Carlo N-Particle eXtended  
(MCNPX) is a software package  
for simulating nuclear processes,  
developed by Los Alamos  
National Laboratory.

Simple calculations took  
about 5 days.

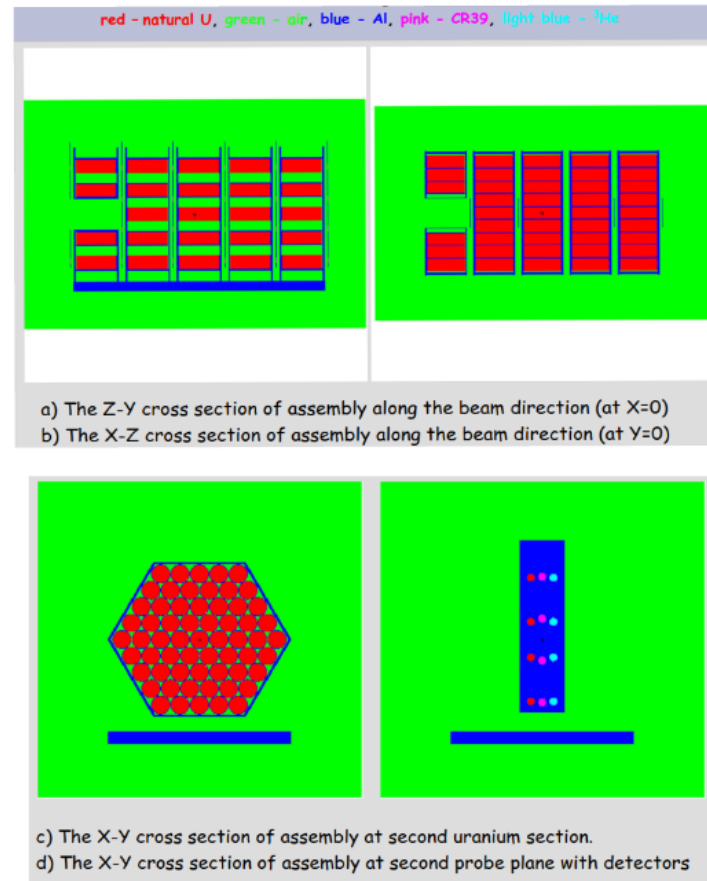
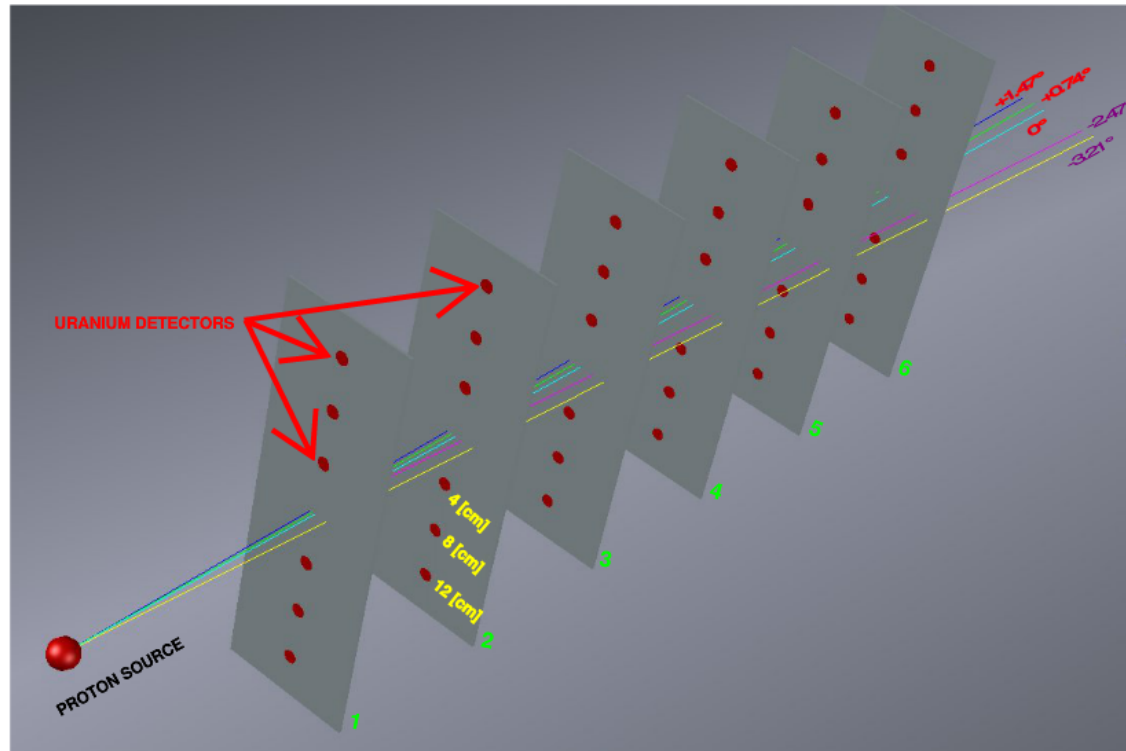


Fig. 7. Geometry of simulation setup.

## How to solve our problem

We recognize that beam of protons can be deflected in x axis.



There is also deflection in y-axis, but it is constant and equal  $1.84^\circ$ .

We calculated 5 options for 5 different angles:

- $-3.21^\circ$
- $-2.47^\circ$
- $0^\circ$
- $0.74^\circ$
- $1.74^\circ$

We chose two best cases:

- $-3.21^\circ$
- $-2.47^\circ$

And conduct further analysis for them.

photo

# Results

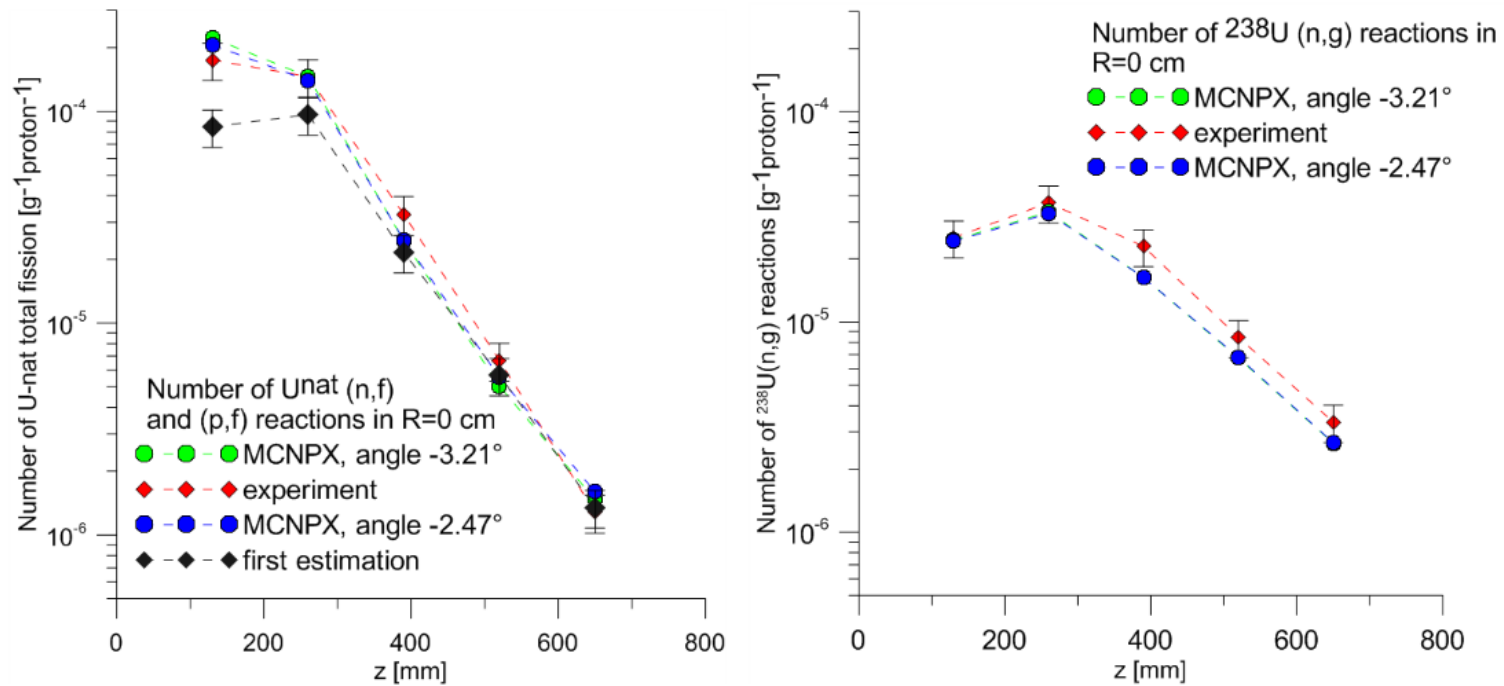


Fig. 8. and Fig. 9.

# Results

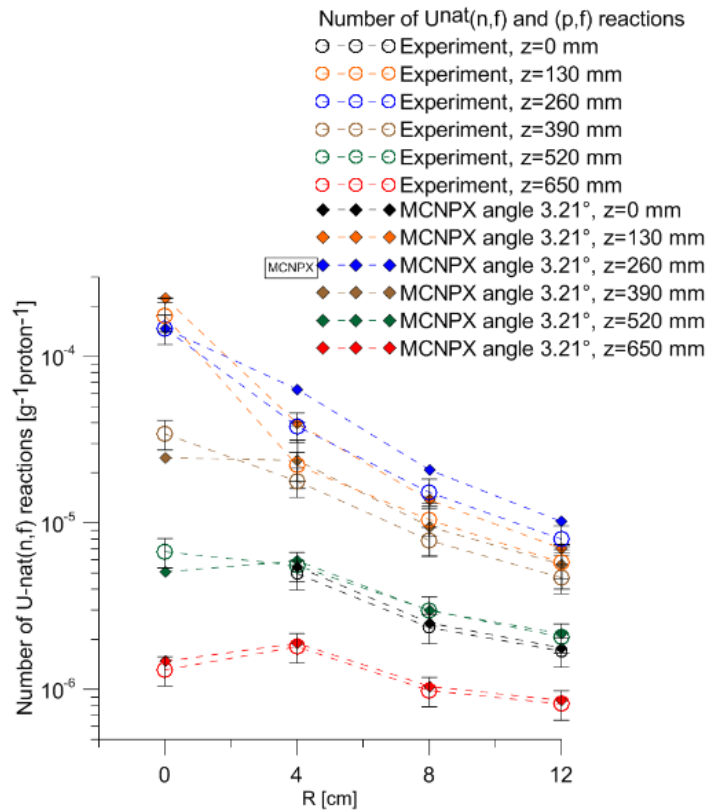


Fig. 10.

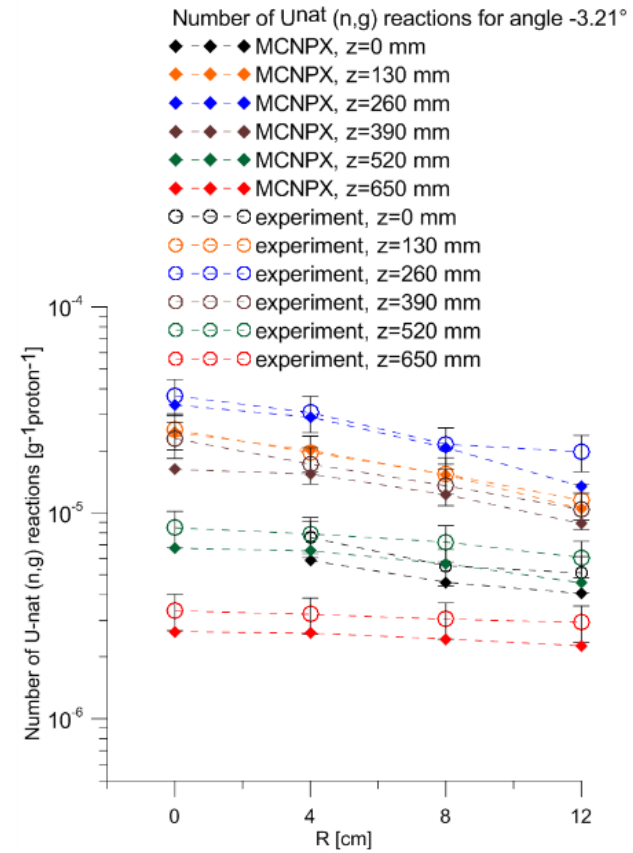


Fig. 11.



# Results

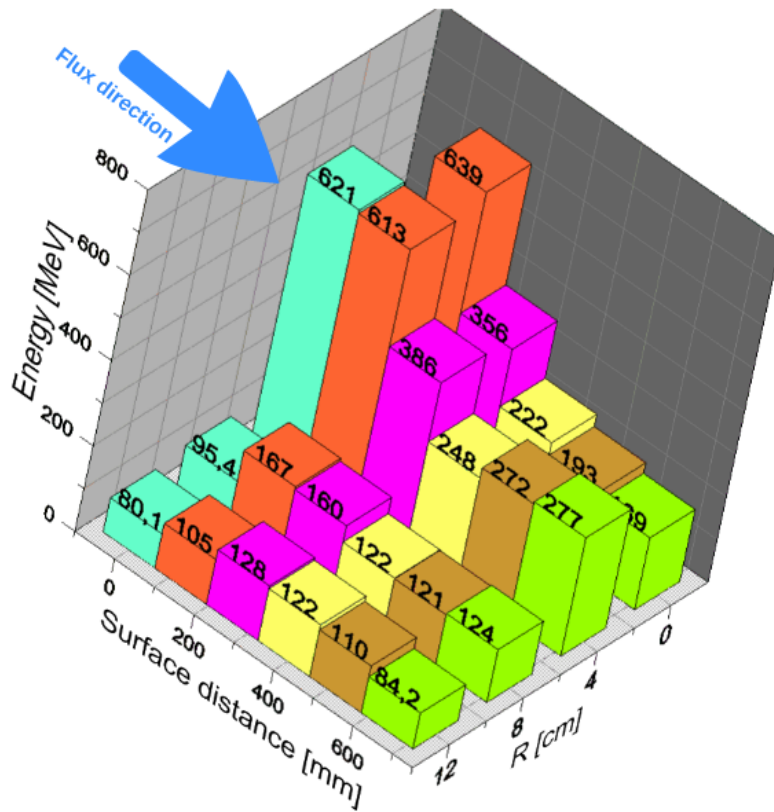


Fig. 12. Average proton energy in detectors for angle = -3.21°.

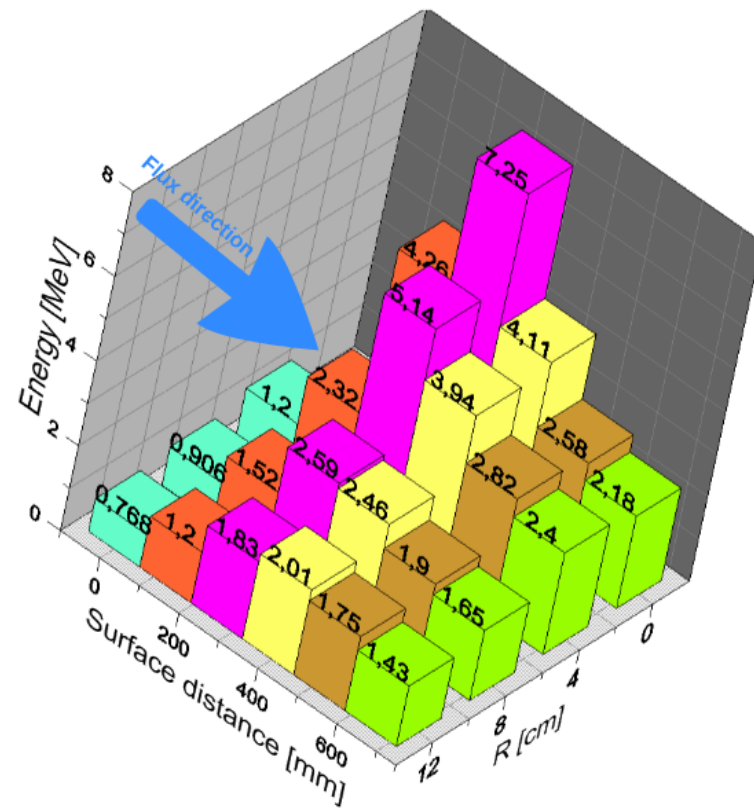
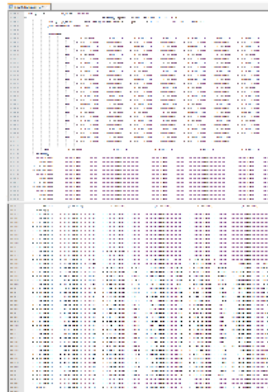


Fig. 13. Average neutron energy in detectors for angle = -3.21°.

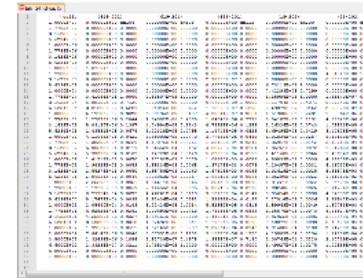
## In conclusion...

- We succeeded in finding out a possible cause of our problem - deflected beam in x-axis.
- We obtained a good agreement of experimental data and calculated results in all detectors, especially on the assembly axis.
- We estimated angle of deflection to be in range between  $-3.21^\circ$  to  $-2.47^\circ$ .
- Computer modeling is much easier process than conducting an actual experiment.
- It is also a great tool to predict results and even upgrade experimental data in terms of quality.

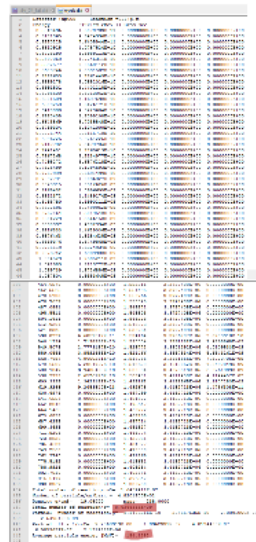
# What analysis look like - "the kitchen"



A screenshot of a data table with multiple columns and rows of numerical data, likely representing simulation results or experimental data.



A screenshot of a data table with multiple columns and rows of numerical data, similar to the top-left table.



A screenshot of a data table with multiple columns and rows of numerical data, similar to the other tables.



```
=====
Name of input filter: 3      filter.dat
Name of detector: 4980
Number of filter data: 45   filter.dat
Name of input filter: 235(p.f)
Name of detector: 4980
Number of cross sect: 64
Name of output filter: 235(p.f)

Total number of reactions/cd= 1.4452411E-07
Total number of reactions/g= 8.4343027E-07
Partial number of reactions/g= 1.1906161E-18  2.4037625E-18  2.8091895E-09
2.5495498E-09
Partial flux (neutrons) 2.785219E-08  1.4062331E-07  4.019408E-07
Partials/cd= 2.191283E-08
Average particle energy (MeV)= 154.1252
```





tally\_24\_full.dat

	cell:	(618<201)	(619<201)	(616<201)	(18<202)	(13<202)
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2	1.0000E-07	0.00000E+00 dn104	0.00000E+00 dn108	0.00000E+00 dn112	0.00000E+00 dn200	0.00000E+00 dn204
3	1.7783E-07	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000
4	3.1623E-07	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000
5	5.6234E-07	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000
6	1.0000E-06	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000
7	1.7783E-06	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000
8	3.1623E-06	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000
9	5.6234E-06	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000
10	1.0000E-05	4.87691E-08 1.0000	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000
11	1.7783E-05	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000	4.94919E-08 1.0000
12	3.1623E-05	0.00000E+00 0.0000	0.00000E+00 0.0000	2.38358E-07 1.0000	0.00000E+00 0.0000	0.00000E+00 0.0000
13	5.6234E-05	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000	6.73113E-08 1.0000	0.00000E+00 0.0000
14	1.0000E-04	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000	7.41293E-08 0.7199	0.00000E+00 0.0000
15	1.7783E-04	3.41096E-08 1.0000	2.53507E-08 1.0000	0.00000E+00 0.0000	3.38986E-08 1.0000	1.51540E-07 0.6167
16	3.1623E-04	6.88155E-08 0.7136	0.00000E+00 0.0000	9.67260E-09 1.0000	7.11794E-07 0.4071	8.57343E-08 0.7451
17	5.6234E-04	3.81885E-07 0.5287	9.34046E-08 0.5672	1.18023E-07 0.6095	5.69079E-07 0.3462	2.93970E-07 0.4014
18	1.0000E-03	6.17136E-07 0.3020	6.89194E-07 0.3487	4.38011E-07 0.3551	1.51908E-06 0.2431	1.58364E-06 0.2187
19	1.7783E-03	1.22829E-06 0.2044	1.54082E-06 0.2305	1.84645E-06 0.2225	5.04182E-06 0.1191	4.39923E-06 0.1176
20	3.1623E-03	5.03120E-06 0.1387	4.04994E-06 0.1343	4.76969E-06 0.1288	1.16326E-05 0.0743	1.05513E-05 0.0826
21	5.6234E-03	1.43591E-05 0.0674	1.22328E-05 0.0795	1.14741E-05 0.0828	3.69495E-05 0.0419	3.40628E-05 0.0448
22	1.0000E-02	4.11069E-05 0.0421	3.69003E-05 0.0470	3.77853E-05 0.0449	1.01836E-04 0.0257	9.14133E-05 0.0271
23	1.7783E-02	1.38390E-04 0.0229	1.17076E-04 0.0251	1.22122E-04 0.0247	3.35967E-04 0.0142	3.12718E-04 0.0147
24	3.1623E-02	5.00523E-04 0.0117	4.36552E-04 0.0132	4.00728E-04 0.0134	1.35751E-03 0.0072	1.31265E-03 0.0073
25	5.6234E-02	5.93318E-04 0.0109	5.14723E-04 0.0120	5.09335E-04 0.0119	1.61168E-03 0.0066	1.49634E-03 0.0068
26	1.0000E-01	1.41215E-03 0.0070	1.17152E-03 0.0079	1.08690E-03 0.0083	4.50893E-03 0.0039	4.19378E-03 0.0041
27	1.7783E-01	1.94329E-03 0.0059	1.55336E-03 0.0068	1.37173E-03 0.0073	7.10457E-03 0.0031	6.46012E-03 0.0033
28	3.1623E-01	2.55279E-03 0.0050	1.95750E-03 0.0060	1.67605E-03 0.0065	1.02619E-02 0.0025	8.89578E-03 0.0027
29	5.6234E-01	2.86914E-03 0.0046	2.08853E-03 0.0057	1.66918E-03 0.0064	1.35280E-02 0.0022	1.11810E-02 0.0024
30	1.0000E+00	2.25592E-03 0.0051	1.56614E-03 0.0065	1.23149E-03 0.0075	1.31221E-02 0.0022	9.64479E-03 0.0025
31	1.7783E+00	1.19115E-03 0.0067	7.14455E-04 0.0095	5.30740E-04 0.0113	1.03243E-02 0.0026	6.14274E-03 0.0031
32	3.1623E+00	8.29354E-04 0.0079	4.46261E-04 0.0119	3.10133E-04 0.0142	9.35654E-03 0.0030	4.82993E-03 0.0035
33	5.6234E+00	5.17473E-04 0.0095	2.51436E-04 0.0152	1.52653E-04 0.0197	7.27014E-03 0.0036	3.36941E-03 0.0041
34	1.0000E+01	2.05440E-04 0.0143	9.22426E-05 0.0234	5.52992E-05 0.0318	3.59969E-03 0.0049	1.50753E-03 0.0060
35	1.7783E+01	6.92929E-05 0.0261	3.00693E-05 0.0413	1.75496E-05 0.0569	1.35570E-03 0.0073	5.45927E-04 0.0099
36	3.1623E+01	4.25800E-05 0.0327	1.99151E-05 0.0500	1.44751E-05 0.0653	9.92922E-04 0.0085	3.88448E-04 0.0119
37	5.6234E+01	3.60306E-05 0.0368	1.92692E-05 0.0541	1.17624E-05 0.0695	9.40077E-04 0.0090	3.40473E-04 0.0127
38	1.0000E+02	1.97567E-05 0.0511	1.02165E-05 0.0787	7.87361E-06 0.0940	6.91408E-04 0.0108	2.24238E-04 0.0162
39	2.0000E+02	7.64149E-06 0.0846	5.07031E-06 0.1102	3.11370E-06 0.1390	4.10805E-04 0.0134	1.14856E-04 0.0229
40	3.5000E+02	1.32496E-06 0.1856	2.51730E-07 0.4578	1.95587E-07 0.7130	1.00769E-04 0.0220	2.40719E-05 0.0451
41	6.6000E+02	2.33238E-07 0.3211	2.73834E-08 1.0000	0.00000E+00 0.0000	3.49927E-05 0.0275	1.00389E-05 0.0560
42	6.8000E+02	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000
43	1.0000E+03	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000	0.00000E+00 0.0000
44						
45						



```

numer kolumny:
3
numer kolumny      3
Name of input file: flux.dat
Name of detector:   dp608
Number of flux data 45
Name of input file: sigma.dat
Name of detector:   238(p.f)
Number of cross sect 61
Name of output file: wynik.dat

Total number of reaction/cm3= 1.6452411E-07
Total number of reaction/g= 8.6364365E-09
Partial number of reaction/g= 1.1486316E-10    3.4557635E-10    2.0891096E-09
2.5495490E-09
Partial flux 1/cm2g= 7.2968319E-08    1.0362331E-07    4.8194488E-07
6.5853652E-07    2.1912888E-06
Average particle energy [MeV]= 154.1252

Kosz      n5.dat      2017-07-17 15:10    PKW.DAT
bilety    okw660-piNC-drc-3372 2017-07-17 13:44    PKW

```



1	Detector :dp608	Reaction =238(p.f)			
2	Energy	Flux[cm-2MeV-1]	Cros.sec		
3	0.5043436	1.5070703E-11	0.0000000E+00	0.0000000E+00	0.0000000E+00
4	0.5131065	4.5474336E-11	0.0000000E+00	0.0000000E+00	0.0000000E+00
5	0.5220215	7.6405944E-11	0.0000000E+00	0.0000000E+00	0.0000000E+00
6	0.5310915	1.0787524E-10	0.0000000E+00	0.0000000E+00	0.0000000E+00
7	0.5403190	1.3989113E-10	0.0000000E+00	0.0000000E+00	0.0000000E+00
8	0.5497068	1.7246311E-10	0.0000000E+00	0.0000000E+00	0.0000000E+00
9	0.5592577	2.0560112E-10	0.0000000E+00	0.0000000E+00	0.0000000E+00
10	0.5689746	2.3931507E-10	0.0000000E+00	0.0000000E+00	0.0000000E+00
11	0.5788603	2.7361449E-10	0.0000000E+00	0.0000000E+00	0.0000000E+00
12	0.5889178	3.0851016E-10	0.0000000E+00	0.0000000E+00	0.0000000E+00
13	0.5991501	3.4401215E-10	0.0000000E+00	0.0000000E+00	0.0000000E+00
14	0.6095600	3.8013062E-10	0.0000000E+00	0.0000000E+00	0.0000000E+00
15	0.6201509	4.1687698E-10	0.0000000E+00	0.0000000E+00	0.0000000E+00
16	0.6309258	4.5426171E-10	0.0000000E+00	0.0000000E+00	0.0000000E+00
17	0.6418880	4.9229604E-10	0.0000000E+00	0.0000000E+00	0.0000000E+00
18	0.6530405	5.3099108E-10	0.0000000E+00	0.0000000E+00	0.0000000E+00
19	0.6643869	5.7035848E-10	0.0000000E+00	0.0000000E+00	0.0000000E+00
20	0.6759304	6.1041000E-10	0.0000000E+00	0.0000000E+00	0.0000000E+00
21	0.6876744	6.5115718E-10	0.0000000E+00	0.0000000E+00	0.0000000E+00
22	0.6996225	6.9261225E-10	0.0000000E+00	0.0000000E+00	0.0000000E+00
23	0.7117782	7.3478784E-10	0.0000000E+00	0.0000000E+00	0.0000000E+00
24	0.7241451	7.7769613E-10	0.0000000E+00	0.0000000E+00	0.0000000E+00
25	0.7367268	8.2134977E-10	0.0000000E+00	0.0000000E+00	0.0000000E+00
26	0.7495272	8.6576218E-10	0.0000000E+00	0.0000000E+00	0.0000000E+00
27	0.7625499	9.1094593E-10	0.0000000E+00	0.0000000E+00	0.0000000E+00
28	0.7757989	9.5691499E-10	0.0000000E+00	0.0000000E+00	0.0000000E+00
29	0.7892781	1.0036827E-09	0.0000000E+00	0.0000000E+00	0.0000000E+00
30	0.8029915	1.0512626E-09	0.0000000E+00	0.0000000E+00	0.0000000E+00
31	0.8169432	1.0996695E-09	0.0000000E+00	0.0000000E+00	0.0000000E+00
32	0.8311372	1.1489174E-09	0.0000000E+00	0.0000000E+00	0.0000000E+00
33	0.8455780	1.1990211E-09	0.0000000E+00	0.0000000E+00	0.0000000E+00
34	0.8602695	1.2499952E-09	0.0000000E+00	0.0000000E+00	0.0000000E+00
35	0.8752164	1.3018548E-09	0.0000000E+00	0.0000000E+00	0.0000000E+00
36	0.8904229	1.3546158E-09	0.0000000E+00	0.0000000E+00	0.0000000E+00
37	0.9058937	1.4082934E-09	0.0000000E+00	0.0000000E+00	0.0000000E+00
38	0.9216333	1.4629036E-09	0.0000000E+00	0.0000000E+00	0.0000000E+00
39	0.9376463	1.5184625E-09	0.0000000E+00	0.0000000E+00	0.0000000E+00
40	0.9539376	1.5749868E-09	0.0000000E+00	0.0000000E+00	0.0000000E+00
41	0.9705119	1.6324934E-09	0.0000000E+00	0.0000000E+00	0.0000000E+00
42	0.9873742	1.6909988E-09	0.0000000E+00	0.0000000E+00	0.0000000E+00
43	1.004529	1.7505211E-09	0.0000000E+00	0.0000000E+00	0.0000000E+00
44	1.021983	1.8110772E-09	0.0000000E+00	0.0000000E+00	0.0000000E+00
45	1.039739	1.8726856E-09	0.0000000E+00	0.0000000E+00	0.0000000E+00
46	1.057804	1.9353645E-09	0.0000000E+00	0.0000000E+00	0.0000000E+00

45	1.033733	1.8728838E-09	0.0000000E+00	0.0000000E+00	0.0000000E+00
46	1.057804	1.9353645E-09	0.0000000E+00	0.0000000E+00	0.0000000E+00
398	454.6570	0.0000000E+00	1.552211	3.3727408E-06	0.0000000E+00
399	462.5565	0.0000000E+00	1.551495	3.3727408E-06	0.0000000E+00
400	470.5933	0.0000000E+00	1.550766	3.3727408E-06	0.0000000E+00
401	478.7697	0.0000000E+00	1.550025	3.3727408E-06	0.0000000E+00
402	487.0881	0.0000000E+00	1.549271	3.3727408E-06	0.0000000E+00
403	495.5511	0.0000000E+00	1.548503	3.3727408E-06	0.0000000E+00
404	504.1611	0.0000000E+00	1.546223	3.3727408E-06	0.0000000E+00
405	512.9207	0.0000000E+00	1.542273	3.3727408E-06	0.0000000E+00
406	521.8325	0.0000000E+00	1.538254	3.3727408E-06	0.0000000E+00
407	530.8992	6.6851517E-11	1.534164	3.3736787E-06	9.3789310E-10
408	540.1234	1.7138398E-10	1.530004	3.3761182E-06	2.4395868E-09
409	549.5078	2.7773137E-10	1.525772	3.3801291E-06	4.0109533E-09
410	559.0553	3.8592693E-10	1.521466	3.3857834E-06	5.6543161E-09
411	568.7687	4.9600241E-10	1.517085	3.3931556E-06	7.3720705E-09
412	578.6509	5.2064797E-10	1.512628	3.4010052E-06	7.8497049E-09
413	588.7047	3.9405498E-10	1.508094	3.4070313E-06	6.0261809E-09
414	598.9333	2.6526176E-10	1.503481	3.4111458E-06	4.1144457E-09
415	609.3395	1.3423132E-10	1.498162	3.4132565E-06	2.1107183E-09
416	619.9266	9.2453540E-13	1.492678	3.4132713E-06	1.4736308E-11
417	630.6976	0.0000000E+00	1.487099	3.4132713E-06	0.0000000E+00
418	641.6557	0.0000000E+00	1.481422	3.4132713E-06	0.0000000E+00
419	652.8042	0.0000000E+00	1.475647	3.4132713E-06	0.0000000E+00
420	664.1465	0.0000000E+00	1.469772	3.4132713E-06	0.0000000E+00
421	675.6858	0.0000000E+00	1.463795	3.4132713E-06	0.0000000E+00
422	687.4255	0.0000000E+00	1.457714	3.4132713E-06	0.0000000E+00
423	699.3693	0.0000000E+00	1.451527	3.4132713E-06	0.0000000E+00
424	711.5206	0.0000000E+00	1.445774	3.4132713E-06	0.0000000E+00
425	723.8830	0.0000000E+00	1.439951	3.4132713E-06	0.0000000E+00
426	736.4602	0.0000000E+00	1.434027	3.4132713E-06	0.0000000E+00
427	749.2560	0.0000000E+00	1.428000	3.4132713E-06	0.0000000E+00
428	762.2740	0.0000000E+00	1.421869	3.4132713E-06	0.0000000E+00
429	775.5182	0.0000000E+00	1.415631	3.4132713E-06	0.0000000E+00
430	788.9926	0.0000000E+00	1.409284	3.4132713E-06	0.0000000E+00
431	802.7010	0.0000000E+00	1.402841	3.4132713E-06	0.0000000E+00
432	816.6477	0.0000000E+00	1.396342	3.4132713E-06	0.0000000E+00
433	830.8367	0.0000000E+00	1.389730	3.4132713E-06	0.0000000E+00
434	Total number of reaction/cm3= 1.6452411E-07				
435	Number of particle/cm*barn = 4.8201300E-02				
436	Density g/cm3= 19.05000 masa= 238.0000				
437	Total number of reaction/g= 8.6364365E-09				
438	Partial number of reaction/g= 1.1486316E-10 3.4557635E-10 2.0891096E-09				
439	2.5495490E-09				
440	Partial flux 1/cm2= 7.2968319E-08 1.0362331E-07 4.8194488E-07				
441	6.5853652E-07 2.1912888E-06				
442	Average particle energy [MeV]= 154.1252				
443					



# THANK YOU!

And we hope we resolved all your doubts

## Sources

- Spallation Physics - An Overview, Gary J. Russel
- Neutron Generation, John M. Carpenter
- Users manual for MCNPX 2.7.0